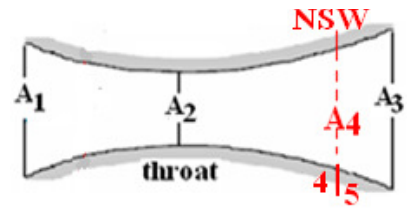


Name: Section:

مطلوب كتابة النتائج وجميع الرسومات فى الجدول وتسليمه مع تقرير به تفاصيل الحسابات

It is required to design all the isentropic air flow conditions in a converging-diverging duct which has the following real dimensions: $A_1=0.5 \text{ m}^2$, $A_2=0.3 \text{ m}^2$ and $A_3=0.7 \text{ m}^2$. The available stagnation conditions are: $P_0=7 \text{ bar}$ & $T_0=600 \text{ K}$. Using attached empirical equations without using any tables, graphs or trial & error, **Complete the Mach number & P design data table:**



Conditions	At inlet A_1	At throat A_2	At exit A_3	Sketch distributions of M # & P along duct axis	
Case (1): Is it choked or non-choked flow?.....	Subsonic inlet $M_1 = 0.25$ $A_1^* = \dots \text{ m}^2$ $P_1 = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	$A_2^* = \dots \text{ m}^2$ $M_2 = \dots$ $P_2 = \dots \text{ bar}$ $P^* = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	Type of flow at exit..... $A_3^* = \dots \text{ m}^2$ $M_3 = \dots$ $P_3 = \dots \text{ bar}$		
Case (2): Is it choked or non-choked flow?.....	Supersonic inlet $M_1 = \dots$ $A_1^* = \text{as case(1)}$ $P_1 = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	$A_2^* = \dots \text{ m}^2$ $M_2 = \dots$ $P_2 = \dots \text{ bar}$ $P^* = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	Type of flow at exit..... $A_3^* = \dots \text{ m}^2$ $M_3 = \dots$ $P_3 = \dots \text{ bar}$		
Case (3): Is it choked or non-choked flow?.....	Subsonic inlet $M_1 = 0.381$ $A_1^* = \dots \text{ m}^2$ $P_1 = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	$A_2^* = \dots \text{ m}^2$ $M_2 = \dots$ $P_2 = \dots \text{ bar}$ $P^* = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	Subsonic exit at $M_3 = \dots$ $P_3 = \dots \text{ bar}$ Supersonic exit $M_3 = \dots$ $P_3 = \dots \text{ bar}$		
Case (4): Is it choked or non-choked flow?.....	Supersonic inlet $M_1 = 1.9798$ $A_1^* = \dots \text{ m}^2$ $P_1 = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	$A_2^* = \dots \text{ m}^2$ $M_2 = \dots$ $P_2 = \dots \text{ bar}$ $P^* = \dots \text{ bar}$ $m = \dots \text{ kg/s}$	Subsonic exit at $M_3 = \dots$ $P_3 = \dots \text{ bar}$ Supersonic exit $M_3 = \dots$ $P_3 = \dots \text{ bar}$		
Case(5) same inlet as in case(3) above but we have normal shock wave at $A_4=0.5 \text{ m}^2$, Is flow choked or not?.....	$M_2 = \dots$, $A_1^* = A_2^* = A_4^* = \dots \text{ m}^2$ & $m = \dots \text{ kg/s}$ Before NSW: $M_4 = \dots$, $P_4 = \dots \text{ bar}$, $P_{O4} = \dots \text{ bar}$ After N.S.W: $M_5 = \dots$, $P_5 = \dots \text{ bar}$, $P_{O5} = \dots \text{ bar}$, $P_{O3} = \dots \text{ bar}$, $A_5^*/A_4^* = \dots$ & $M_3 = \dots$, $P_3 = \dots \text{ bar}$	$A_2^* = \dots \text{ m}^2$ $M_2 = \dots$ $P_2 = \dots \text{ bar}$ $P^* = \dots \text{ bar}$ $m = \dots \text{ kg/s}$			
T-S diagram of case-1	T-S diagram of case-2	T-S diagram of case-3	T-S diagram of case-4	T-S diagram of case-5	

Some Useful Gas Dynamics Relations

Stagnation Reference States:

$$\frac{T_o}{T} = 1 + \frac{\gamma - 1}{2} M^2 \dots\dots\dots, \quad \frac{P_o}{P} = \left\{ 1 + \frac{\gamma - 1}{2} M^2 \right\}^{\frac{\gamma}{\gamma - 1}}$$

For Isentropic Flow in a Variable Area Duct :

$$\frac{A}{A^*} = \frac{1}{M} \left(\frac{2 + (\gamma - 1)M^2}{(\gamma + 1)} \right)^{\frac{(\gamma + 1)}{2(\gamma - 1)}} \dots\dots\dots, \quad \frac{A}{A^*} = \frac{(1 + 0.2M^2)^3}{1.728 * M} \dots\dots\dots \text{for } \gamma = 1.4$$

$$M \approx \frac{1 + 0.27(A/A^*)^{-2}}{1.728(A/A^*)} \dots\dots\dots \text{for .subsonic .flow ... } \gamma = 1.4 \dots \text{and } \longrightarrow 1.34 < A/A^* < \infty$$

$$M \approx 1 - 0.88 \{ \ln(A/A^*) \}^{0.45} \dots\dots\dots \text{for .subsonic .flow ... } \gamma = 1.4 \dots \text{and } \longrightarrow 1.0 < A/A^* < 1.34$$

$$M \approx 1 + 1.2(A/A^* - 1)^{1/2} \dots\dots\dots \text{for .sup ersonic .flow ... } \gamma = 1.4 \dots \text{and } \longrightarrow 1.0 < A/A^* < 2.9$$

$$M \approx [216(A/A^*) - 254(A/A^*)^{2/3}]^{1/5} \dots\dots\dots \text{for .sup ersonic .flow ... } \gamma = 1.4 \dots \text{and } \longrightarrow 2.9 < A/A^* < \infty$$

For Normal shock Wave :

$$\frac{P_2}{P_1} = \frac{1}{\gamma + 1} [2\gamma M_1^2 - (\gamma - 1)] = \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2} \dots\dots\dots, \quad M_2^2 = \frac{(\gamma - 1)M_1^2 + 2}{2\gamma M_1^2 - (\gamma - 1)}$$

$$\frac{\rho_2}{\rho_1} = \frac{V_1}{V_2} = \frac{(\gamma + 1)M_1^2}{(\gamma - 1)M_1^2 + 2} \dots\dots\dots, \quad \frac{T_2}{T_1} = \left[2 + (\gamma - 1)M_1^2 \right] \frac{2\gamma M_1^2 - (\gamma - 1)}{(\gamma + 1)^2 M_1^2}$$

$$\frac{P_{o2}}{P_{o1}} = \frac{\rho_{o2}}{\rho_{o1}} = \left[\frac{(\gamma + 1)M_1^2}{(\gamma - 1)M_1^2 + 2} \right]^{\frac{\gamma}{\gamma - 1}} \left[\frac{\gamma + 1}{2\gamma M_1^2 - (\gamma - 1)} \right]^{\frac{1}{\gamma - 1}} \dots\dots\dots, \quad \frac{A^*_2}{A^*_1} = \frac{M_2}{M_1} \left[\frac{(\gamma - 1)M_1^2 + 2}{(\gamma - 1)M_2^2 + 2} \right]^{\frac{\gamma + 1}{2(\gamma - 1)}}$$

For Fanno-Line Flow :

$$\frac{\bar{f} \cdot L^*}{D} = \frac{1 - M^2}{\gamma M^2} + \frac{\gamma + 1}{2\gamma} \ln \left[\frac{(\gamma + 1)M^2}{2 + (\gamma - 1)M^2} \right] \dots\dots\dots, \quad \frac{\bar{f} \cdot \Delta L}{D} = \left(\frac{\bar{f} \cdot L^*_1}{D} \right) - \left(\frac{\bar{f} \cdot L^*_2}{D} \right)$$

$$\frac{T}{T^*} = \frac{a^2}{a^{*2}} = \frac{\gamma + 1}{2 + (\gamma - 1)M^2} \dots\dots\dots, \quad \frac{P}{P^*} = \frac{1}{M} \left[\frac{\gamma + 1}{2 + (\gamma - 1)M^2} \right]^{1/2}$$

$$\frac{\rho}{\rho^*} = \frac{V^*}{V} = \frac{1}{M} \left[\frac{2 + (\gamma - 1)M^2}{\gamma + 1} \right]^{1/2} \dots\dots\dots, \quad \frac{P_o}{P_o^*} = \frac{\rho_o}{\rho_o^*} = \frac{1}{M} \left[\frac{2 + (\gamma - 1)M^2}{\gamma + 1} \right]^{\frac{\gamma + 1}{2(\gamma - 1)}}$$

For Isothermal Flow with Friction:

$$\frac{\bar{f} \cdot L_{\max}}{D} = \frac{1 - \gamma M^2}{\gamma M^2} + \ln(\gamma M^2) \dots\dots\dots, \quad \frac{P_1}{P'} = \frac{1}{M_1 \cdot \gamma^{0.5}} \dots\dots\dots, \quad \frac{V_1}{V'} = \frac{\rho'}{\rho_1} = M_1 \cdot \gamma^{0.5}$$

$$\frac{P_1}{P_2} = \frac{\rho_1}{\rho_2} = \frac{V_2}{V_1} = \frac{M_2}{M_1} \dots\dots\dots, \quad G^2 = (\dot{m}/A)^2 = \frac{P_1^2 - P_2^2}{R \cdot T [(\bar{f} \cdot L/D) + 2 \ln(P_1/P_2)]}$$

For Rayleigh Line Flow :

$$\frac{T_o}{T_o^*} = \frac{(\gamma + 1)M^2 [2 + (\gamma - 1)M^2]}{(1 + \gamma \cdot M^2)^2} \dots\dots\dots, \quad \frac{T}{T^*} = \frac{(\gamma + 1)^2 \cdot M^2}{(1 + \gamma \cdot M^2)^2} \dots\dots\dots, \quad \frac{P}{P^*} = \frac{\gamma + 1}{1 + \gamma \cdot M^2}$$

$$\frac{V}{V^*} = \frac{\rho^*}{\rho} = \frac{(\gamma + 1)M^2}{1 + \gamma \cdot M^2} \dots\dots\dots, \quad \frac{P_o}{P_o^*} = \frac{\gamma + 1}{1 + \gamma \cdot M^2} \left[\frac{2 + (\gamma - 1)M^2}{\gamma + 1} \right]^{\frac{\gamma}{\gamma - 1}}$$